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8 **Predicting effective thermal conductivity in sand using an artificial neural network with**  
9 **multiscale microstructural parameters**

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11 Author 1

12 Wenbin Fei, PhD, ME, BE

13 Department of Infrastructure Engineering, The University of Melbourne, Parkville, Australia

14 ORCID: 0000-0002-9275-8403

15  
16 Author 2

17 Guillermo A. Narsilio✉, PhD, MSc (Math), MSc (CE), CEng

18 Department of Infrastructure Engineering, The University of Melbourne, Parkville, Australia

19 ORCID: 0000-0003-1219-5661

20  
21 Author 3

22 Mahdi M. Disfani, PhD, MSc, BSc

23 Department of Infrastructure Engineering, The University of Melbourne, Parkville, Australia

24 ORCID: 0000-0002-9231-8598

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37  
38  
39  
40 Full contact details of the corresponding author

41 Guillermo A. Narsilio, Deputy Head of Department (Research) & Associate Professor

42 Engineering Block B 208, Department of Infrastructure Engineering, The University of  
43 Melbourne, Parkville, VIC 3010, Australia

44 Email: narsilio@unimelb.edu.au, Phone: +61 (3) 8344 4659, Fax: +61 (3) 8344 4616

45     ***Abstract***

46     Accurate and efficient prediction of thermal conductivity of sands is challenging due to the  
47 variations in particle size, shape, connectivity and mineral compositions, and external  
48 conditions. Artificial Neural Networks (ANN) models have been used to predict the effective  
49 thermal conductivity but they have not considered variables related to particle connectivity.  
50 This work uses computed tomography (CT) scanned images of four dry sands and network  
51 analysis to redress this significant shortcoming. Here sands are represented as networks of  
52 nodes (grains) and edges (interparticle contacts or/and small gaps between neighbouring  
53 particles) to extract network features that characterise interparticle connectivity. A network  
54 feature – *weighted coordination number* (WCN) capturing both particle connectivity and  
55 contact area – was found to be a good predictor of effective thermal conductivity in dry  
56 materials. Roundness, sphericity, solid particle thermal conductivity and porosity are other  
57 input parameters rigorously selected for an ANN model that predicts well the effective thermal  
58 conductivity of sands.

59     ***Keywords:*** Machine learning; Heat transfer; Thermal network model; Microstructure;  
60 Micro-CT.

## 61 1 Introduction

62 Granular materials are engaged in numerous applications such as geothermal engineering  
63 [1], petroleum and gas extraction [2], carbon dioxide geological storage [3] and pebble bed  
64 reactors [4]. In these projects, heat transfer is one of the processes that dominate project design  
65 and capital costs. As effective thermal conductivity ( $\lambda_{eff}$ ) indicates the ease of heat transfer, its  
66 accurate and efficient prediction is essential. However, the prediction is challenging due to the  
67 complex microstructure of granular materials and external boundary conditions [5, 6]. The  
68 microstructure can be characterised at different scales, such as particle size, shape, gradation  
69 and minerality at the microscale (particle scale); particle connectivity [7, 8] at the mesoscale  
70 and porosity at the macroscale. Work by van Antwerpen et al. [9], Abdulagatova et al. [10] and  
71 Abyzov et al. [11] investigated a number of  $\lambda_{eff}$  models against experimental data and found  
72 some models simplify granular materials as packings of spheres, ellipsoids or parallel cylinders  
73 (regular geometrical forms), which limited their applicability to natural sands. Moreover,  
74 models characterise packing structure using porosity alone are insufficient [9] and  
75 microstructural parameters about grain-grain resistance [10] and contact area [11, 12] have not  
76 been incorporated in  $\lambda_{eff}$  models although they are important to  $\lambda_{eff}$  prediction [13]. In addition,  
77 particle connectivity, i.e., microstructural contact topology related to thermo-mechanical  
78 response [14], has rarely been quantified except for using coordination number which is  
79 defined as the number of neighbouring particles in contact with a given particle.

80 Recently, researchers abstracted granular materials as contact networks and thermal  
81 networks by creating nodes for particles and edges for interparticle contacts (contact networks),  
82 and with the addition of near-contacts which represent the small gaps between neighbouring  
83 particles (thermal networks) [15]. Then based on complex network theory [16], contact area or  
84 thermal conductance can be added as a weight to each edge in the network to eventually identify  
85 a single mesoscale network feature which can characterise both the particle connectivity and  
86 contact quality. One such feature from the contact network is the *weighted degree*, which  
87 represents an enhanced version of a coordination number that accounts for the contact area of  
88 each interparticle contact. Hence, while coordination numbers only count the number of  
89 neighbouring particles of a target particle, the weighted coordination number (WCN) quantifies  
90 both the contact number (particle connectivity) and contact area (contact quality). The physical  
91 meaning of the WCN is the total contact area of a target particle to its neighbours.

92 Numerical simulation methods such as finite element methods (FEM) [17], discrete element  
93 methods (DEM) [18] and lattice Boltzmann methods (LBM) [19] can be used to estimate  $\lambda_{eff}$

94 with a more detailed complex microstructure involved in the process. However, these  
95 approaches require solving a system of partial differential equations and the computations are  
96 generally time-consuming [14, 20]. On the other hand, physical experiments such as thermal  
97 needle probe test are commonly undertaken to measure  $\lambda_{eff}$  [21], but one of the drawbacks is  
98 that accurate measurement needs relatively large undisturbed samples (150 mm long, 50 mm  
99 in diameter as a minimum) which may be difficult to obtain. The aim of this paper is to develop  
100 a model that can predict  $\lambda_{eff}$  accurately and computationally efficiently, even from very small  
101 samples.

102 Machine learning techniques have enabled substantial advances in data-driven approaches  
103 throughout academia and industry. In the material sciences, materials informatics combine  
104 machine learning, Bayesian optimisation and Monte Carlo tree searches in an attempt to  
105 address the challenge of rapidly finding optimal materials [22]. A limited number of studies  
106 have also used machine learning to predict  $\lambda_{eff}$  of sphere packings [14, 23], equation-based  
107 irregular materials [20] and sands [24]. The input parameters for the machine learning models  
108 in these works include porosity, particle size, component content, the thermal conductivity of  
109 solid and interstitial gas, temperature and loadings. Although these parameters are measurable  
110 in a laboratory [25, 26], bypassing a detailed understanding of structural arrangements and  
111 physical mechanisms may result in the differences observed between calculations and  
112 measurements [9, 13]. Hence, it is necessary to include particle connectivity parameters and  
113 the variables detailed above, in machine learning models that investigate heat transfer.

114 This work intends to predict  $\lambda_{eff}$  accurately and efficiently by developing an ANN model  
115 using important and non-redundant inputs. Here we justify the selection of average WCN  
116 ( $WCN_{ave}$ ) which quantifies the topological structure in sands and other microstructural  
117 variables including particle diameter, three-dimensional sphericity and roundness as input  
118 parameters in the ANN model. Computed tomography (CT) scanned images of four dry sands  
119 that varied in shape, size and endured external loads are used to calculate these parameters. A  
120 recently developed in-house thermal conductance model (TCNM) computed the  $\lambda_{eff}$  acting as  
121 the output parameter in the ANN model [27, 28] alongside complementary experimental  
122 measurements. TCNM mitigates the overestimation of  $\lambda_{eff}$  possibly induced by the particle  
123 volume effect [29] from threshold segmentation, and the variations of  $\lambda_{eff}$  estimation for  
124 different particle arrangements without additional disturbance of samples that result from  
125 insertion of thermal probes.

## 126 2 Artificial neural network models

127 Artificial neural network (ANN) is at the core of deep Machine Learning (ML) techniques  
128 and has managed to render high accuracy in image classification (e.g., Google Images), voice  
129 recognition (e.g., Apple's Siri) and learning (e.g., AlphaGo). The ANN was inspired by the  
130 architecture of the human brain and its architecture composites of an input layer, one or more  
131 hidden layers and an output layer. Each layer has one or more neurons (units/nodes), with the  
132 neurons in different layers connected by edges. As this work attempts to find an accurate and  
133 efficient model to predict  $\lambda_{eff}$ , the neurons in the input layer could be microstructural variables  
134 while the neuron in the output layer is  $\lambda_{eff}$ . Non-linear functions (activation functions) with  
135 weights that correspond to the neurons in the previous layer compute the neurons in the latter  
136 layer. This paper employs the ReLU activation function embedded in Python library  
137 TensorFlow and Keras for the hidden layers due to its high efficiency and general applicability  
138 [30]. In addition to the selection of a robust activation function, an appropriate optimiser can  
139 also adjust the weights and learning rates. This work uses Adam optimisation because it is an  
140 adaptive learning rate algorithm and has several advantages of other optimisation algorithms  
141 such as Momentum optimisation and RMSProp [30].

### 142 2.1 Input parameters determination

143 Even though ANN performs well in solving complex problems, feeding input features  
144 without discretion is not recommended. Sometimes, a larger number of input features might  
145 lead to overfitting, making the trained model only fit specific data [31]. Hence, feature selection  
146 and reduction are usually conducted to find the most relevant and least redundant input features  
147 before training a machine learning model. This section presents a review of the heat transfer  
148 mechanisms and  $\lambda_{eff}$  models to justify the inputs selected in this work.

149 Heat transfer in gas-stagnant granular materials occurs via four critical pathways: (1) heat  
150 conduction within solid particles; (2) heat conduction via interparticle contacts; (3) heat  
151 conduction via particle-gas-particle; (4) heat radiation across the solid surface and is negligible  
152 when the temperature is below 600° [10]. Since the thermal conductivity of the solid is two  
153 orders of magnitude larger than air and this work focuses on the samples at room temperature,  
154 heat travels via the first two mechanisms is known to be more significant for dry soils [32].  
155 Therefore, the ANN model in this work incorporates parameters that relate to the particle and  
156 interparticle contacts. Particle diameter should be an input parameter since it relates to the  
157 distance that heat transfers within the particles, so is the solid thermal conductivity controlling  
158 the ease of heat transfer in the particle. In terms of a parameter related to interparticle contact,

159 the  $WCN_{ave}$  was identified as a good candidate [15] due to its capacity to capture both the  
 160 existence of interparticle contacts but also the area of contact.

161 Selection of optimal input parameters for the ANN model involved a critical analysis of the  
 162 existing parameter used in  $\lambda_{eff}$  models. The majority of  $\lambda_{eff}$  models use porosity and the thermal  
 163 conductivity of different phases [9-11]. Some complex  $\lambda_{eff}$  models in Table 1 also consider  
 164 particle/pore shape which affects heat transfer [33] and mechanical behaviour [34] of granular  
 165 materials. Eq. (1) introduces a parameter  $B$  to adjust the particle shape while Eq. (2) and Eq.  
 166 (3) employ an aspect ratio to characterise the shape of the particle and/or pore. However, these  
 167 are only applicable to particles with regular shapes.

168

169 Table 1 Summary of effective thermal conductivity models that consider particle/pore shape

Reference	
Zehner and Schlunder [35]	$\frac{\lambda_{eff}}{\lambda_f} = 1 - \sqrt{1 - \phi} + \frac{2\sqrt{1-\phi}}{1-\xi B} \left[ \frac{(1-\xi)B}{(1-\xi B)^2} \ln\left(\frac{1}{\xi B}\right) - \frac{B+1}{2} - \frac{B-1}{1-\xi B} \right],$ $\xi = \frac{\lambda_f}{\lambda_s}, r^2 + \frac{z^2}{[B-(B-1)z]^2} = 1.$ <p><math>r</math> and <math>z</math> are the radii of the particle in two principal axes.  <math>B</math> is the shape factor. The particle becomes the <math>z</math>-axis with no solid volume when <math>B \rightarrow 0</math>, a sphere when <math>B \rightarrow 1</math> and a cylinder when <math>B \rightarrow \infty</math>.</p>
Fricke [36]	$\frac{\lambda_{eff}}{\lambda_s} = \frac{(1-\phi)(1-\xi)+\xi\beta\phi}{(1-\phi)(1-\xi)+\beta\phi}, \xi = \frac{\lambda_f}{\lambda_s},$ <p><math>\beta</math> is related to <math>\xi</math> and aspect ratio.</p>
Keller et al. [37]	$\lambda_{eff} = \lambda_s \left[ 1 + \frac{\alpha_p}{\alpha_s} \left( \frac{b}{a} \right)^2 \left( 2 - \frac{b/a}{(1-b/a)^2} \right) \right]^{-1}, \phi = \frac{\alpha_p}{\alpha_s} \left( \frac{b}{a} \right)^2 \left( 2 - \frac{b}{a} \right),$ <p><math>\alpha_p</math> is the aspect ratio of the pore  <math>\alpha_s</math> is the aspect ratio of solid (grain)  <math>b</math> is the pore radius while <math>a</math> is the grain radius.</p>

170  $\lambda_s$  is the thermal conductivity of solid and  $\lambda_f$  is the thermal conductivity of gas/fluid in the void space,

171  $\phi$  is porosity.

172

173 Since aspect ratio cannot adequately cover the shape of all irregular particle/pores [33], three-  
 174 dimensional (3D) sphericity ( $S$  in Eq. (4)) and roundness ( $R$  in Eq. (5)) were used in this work  
 175 to describe the particle shape, details of computational steps can be found in [33]:

$$S = \frac{36\pi V^2}{SA^3} \quad (4)$$

$$R = \frac{\sum r_i/N}{r_{max-in}} \quad (5)$$

176 where  $V$  is particle volume,  $SA$  is particle surface area,  $r_i$  is the radius of each corner [33],  $N$  is  
 177 the total number of corners and  $r_{max-in}$  is the radius of the largest sphere in the particle.

178 Selection of particle size, the thermal conductivity of solid and fluid/gas,  $WCN_{ave}$ , 3D  
179 sphericity and roundness, and porosity as sensible candidates for input parameters in the ANN  
180 model considered the analysis above.

## 181 2.2 Performance indicator

182 Data used for ANN modelling is typically divided into three sets: a training set, a validation  
183 set and a test set when embarking in supervised ML. The training set first trains the ML models  
184 which are evaluated to select the one that has the best performance on the validation set. The  
185 test set then evaluates the performance of the final model.

186 Quantifications of the evaluations can use either the mean square error (MSE) or correlation  
187 coefficient ( $R^2$ ). MSE measures the *standard deviation* of the errors that a model makes in its  
188 predictions, with the preferred application [30] for regression problems. In contrast,  $R^2$  usually  
189 quantifies the linear correlation between the predicted value and actual value. It has a range  
190 from 0 to 1, where 0 signifies no relationship while 1 indicates a perfect fit. Accordingly, MSE  
191 was employed in this study to monitor the performance of the ANN model when tuning  
192 hyperparameters (e.g., the number of nodes in each layer) to select models with  $R^2$  used to  
193 present the general performance of the ANN model.

## 194 3 Data collection

### 195 3.1 Materials

196 Four sands varying in particle shape were sent to the Australian Synchrotron, Imaging and  
197 Medical BeamLine (IMBL) for CT scanning at a pixel size of  $13 \mu m$ . Figure 1 shows a  
198 selection of the acquired images. Glass beads display the roundest particles while the particles  
199 in the Ottawa sand are more irregular but still have round corners. Compared to the particles in  
200 the Ottawa sand, particles in the angular sand are even more irregular and have sharp corners.  
201 Lastly, particles made from crushing schist have the most irregular shape, with half of these  
202 platy and elongated.

203

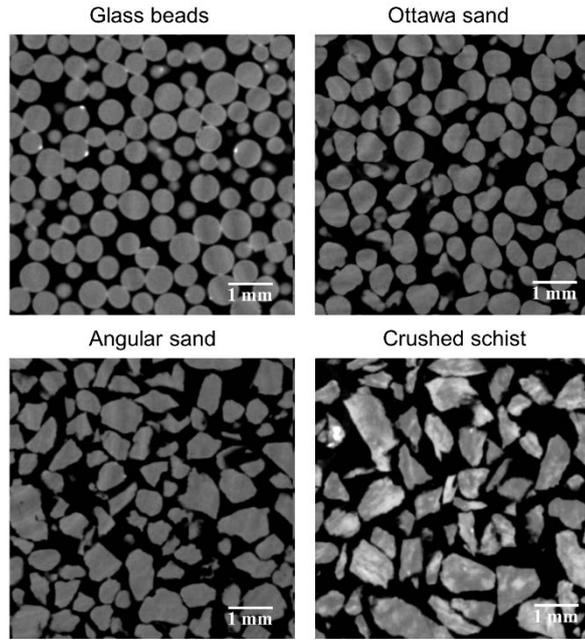


Fig. 1. Selected micro-CT slide images of four sands. Images show the variations in particle shape.

Different particle sizes were chosen and axial loads were applied to sands in Fig. 1 using a rigid wall cell to further vary porosity and particle arrangement (Table 2). Hence, more data were obtained to train a universal ANN. Calculations of the equivalent particle size used CT images, consistent with previous research [27]. The samples shown in Fig. 1 correspond to GB-L, OS, AS-L and CS-M without axial stress in Table 2 and have similar equivalent  $D_{50}$ .

Table 2 Particle size and axial compression stresses applied to each sample

Sand	Sample name	Particle size (mm) <sup>a</sup>	Particle size (mm) <sup>b</sup>	Equivalent $D_{50}$ (mm) <sup>b</sup>	Axial Stress (MPa)
Glass beads	GB-S	0.20-0.30	0.12-0.37	0.24	0, 2.0, 6.1, 10.2
	GB-N	0.50	0.33-0.68	0.54	0, 2.0, 6.1, 10.2
	<b>GB-L</b>	<b>0.50-0.70</b>	<b>0.40-0.80</b>	<b>0.60</b>	<b>0, 2.0, 6.1, 10.2, 20.4, 40.7</b>
Ottawa sand	<b>OS</b>	<b>0.60-0.85</b>	<b>0.58-0.94</b>	<b>0.76</b>	<b>0, 2.0, 6.1, 10.2, 20.4, 40.7</b>
Angular sand	AS-P	0.15-0.30	0.12-0.41	0.24	0
	AS-M	0.43-0.60	0.32-0.64	0.48	0, 2.0, 6.1, 10.2, 20.4, 40.7
	<b>AS-L</b>	<b>0.60-1.18</b>	<b>0.39-0.99</b>	<b>0.68</b>	<b>0, 2.0, 6.1, 10.2, 20.4, 40.7</b>
Crushed schist	CS-S	0.30-0.50	0.17-0.61	0.39	0, 2.0, 6.1, 10.2
	CS-M	0.50-1.18	0.23-0.95	0.58	0

<sup>a</sup> Particle size from sieve analysis

<sup>b</sup> Particle size calculated based on CT reconstructed sample.

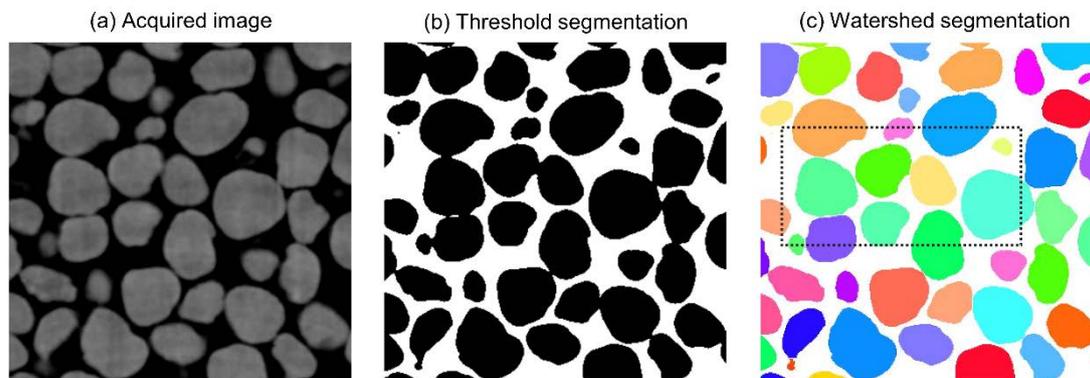
216 3.2 *Microstructural variables*

217 This section briefly introduces the procedure used to obtain the aforementioned particle size,  
218 WCN, 3D sphericity, 3D roundness and porosity.

219 3.2.1 *Image processing*

220 The CT scanning resulted in sequential images with a pixel size of  $13 \mu\text{m}$ . Selection of four  
221 regions of interest (ROI) with a dimension of  $4.55 \times 4.55 \times 4.55 \text{ mm}$  in each image stack  
222 eliminated the effect of potential heterogeneity. Fig. 2 (a) shows a cross-section of the ROI  
223 after applying a 3D median filter. Then a commonly used Otsu threshold segmentation  
224 algorithm [38] distinguished the solid phase (in black) and air phase (in white) as shown in Fig.  
225 2 (b). The adjacent particles in Fig. 2 (b) remain connected and required ‘splitting’ to achieve  
226 the properties (i.e., particle size, shape and WCN) of each particle using watershed  
227 segmentation. Meanwhile, each particle was assigned a unique identifier (ID) and rendered by  
228 random colour as shown in Fig. 2 (c). The Taubin smooth algorithm smoothed out each particle  
229 surface to compute particle volume, particle surface area, 3D sphericity and roundness  
230 following the steps detailed in a recent work [33]. Equivalent particle size calculations used  
231 the particle volume, with porosity computed using the volumes of all the particles and the  
232 known dimension of the ROI.

233



234

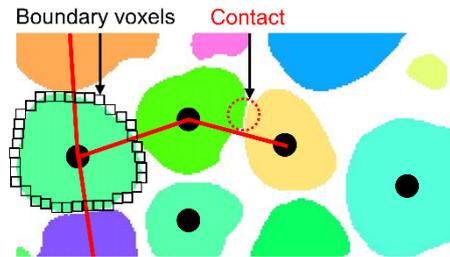
235 Fig. 2. Overview of key steps in image processing to identify individual particles

236 3.2.2 *Weighted coordination number (WCN)*

237 Classical coordination number quantifies the contact number of a particle, a weighted  
238 coordination number (WCN) weights each interparticle contact by the contact area. Hence,  
239 WCN can capture both the existence of contacts and contact area. WCN is termed weighted  
240 degree in complex network theory [16] and can be computed after network constructions. For  
241 each sample in this work, a contact network was constructed by creating a node at the centroid

242 of each particle and an edge for each interparticle contact, as shown in Fig. 3. To identify the  
 243 interparticle contacts, boundary voxels were recognised first if the voxels in a particle are  
 244 adjacent to anything else that was not in the same particle. The average coordinate of the  
 245 boundary voxels can help to locate the centroid of each particle. Furthermore, if boundary  
 246 voxels bordered on another particle, these were identified as interparticle contact voxels and  
 247 further used to estimate the interparticle contact area.

248



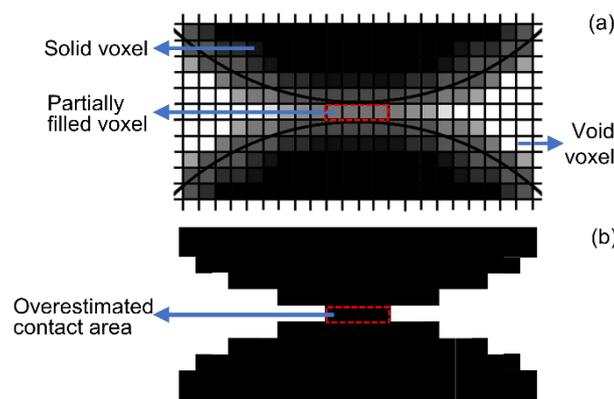
249

250 Fig. 3. Contact network construction for a sample (detailed from the dashed rectangle in Fig. 2 (c))

251

252 A simple way to calculate the interparticle contact area is to directly count the number of  
 253 interparticle contact voxels but this may result in an overestimation after threshold  
 254 segmentation due to partial volume effects [29]. Each pixel in the CT image shown in Fig. 4  
 255 (a) has its own grayscale. Black and white voxels indicate solids and voids, whereas other  
 256 voxels are “grey”. Some of these grey voxels at the 1-pixel gap between the two particles (Fig.  
 257 4 (a)) are incorrectly identified as contacts, which will result in overestimations of both the  
 258 contact area and  $\lambda_{eff}$ .

259



260

261 Fig. 4. CT image of two spheres with a voxel gap. This image displays some partially filled voxels  
 262 (a) incorrectly identified as contact areas after (b) threshold segmentation.

263

264 To correct the interparticle contact area, a penalty factor considering the grayscale of these  
 265 partially filled voxels was introduced. The corrected interparticle contact area  $A^C$  was  
 266 computed as the sum of  $A_{i,j,k}^v$  weighed by the  $\tau^{\text{th}}$  power of the ratio of grayscale values of  
 267 individual interparticle voxels  $g_{(i,j,k)}$  to the maximum grayscale value among all interparticle  
 268 voxels (Eq. (6)). The penalty factor  $\tau$  was set at 10 after the calibration of the  $\lambda_{\text{eff}}$  of sphere  
 269 packings with the result from a theoretical thermal network model [28, 39]:

$$A^C = \sum_{i,j,k} A_{i,j,k}^v = \sum_{i,j,k} \left[ \left( \frac{g_{(i,j,k)}}{\max[g_{(i,j,k)}]} \right)^\tau L_v^2 \right] \quad (6)$$

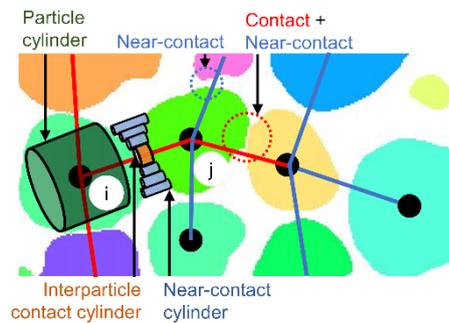
270 where  $L_v$  is the length of a voxel, which is  $13 \mu\text{m}$  in this work.

271 Once the contact network was constructed and interparticle contact area calculated, a  
 272 computationally efficient Python library *graph-tool* [40] calculated the WCN (i.e., *degree* in  
 273 the terminology of complex network theory with the addition of the interparticle contact area  
 274 to each corresponding edge). The degree of a node is the total number of its attached edges,  
 275 whereas the weighted degree of a node is equal to the sum of weights at the attached edges  
 276 [16].

### 277 3.3 Effective thermal conductivity estimations

#### 278 3.3.1 Effective thermal conductivity from thermal conductance network model (TCNM)

279 In order to calculate  $\lambda_{\text{eff}}$ , the contact network in Fig. 3 can be extended to a thermal network  
 280 by considering the small gaps as near-contacts (i.e., the blue edges in Fig. 5), which correspond  
 281 to particle-gas-particle heat conduction. A near-contact was identified if the distance between  
 282 the boundary voxels of two adjacent particles was shorter than the average particle radius [27,  
 283 28]. Then a TCNM model was generated by calculating the thermal conductance at three main  
 284 heat transfer paths (i.e., through the particles, interparticle contacts and near-contacts), which  
 285 is valid for dry granular materials at room temperature.



286  
 287 Fig. 5. Thermal network construction. Red edges represent interparticle contacts while blue edges  
 288 indicate near-contacts. An equivalent particle cylinder (dark green), an interparticle contact cylinder  
 289 (orange) and a series of near-contact cylinders (light blue) are used to calculate thermal conductance

290 through the particle, interparticle contact and near-contact. The process is repeated for all particles  
 291 within the granular material.

292

293 Figure 5 presents three types of equivalent material cylinders that correspond to the three  
 294 heat transfer mechanisms and are used to calculate the thermal conductance. The thermal  
 295 conductance  $C_{cy}$  of a cylinder with a thermal conductivity  $\lambda_{cy}$ , cross-section area  $A^{cy}$  and length  
 296  $L^{cy}$  is computed as  $C_{cy} = \lambda_{cy} A^{cy} / L^{cy}$ . Hence, the thermal conductance  $C^P$  through an equivalent  
 297 particle cylinder (the dark green cylinder in Fig. 5) was calculated as the following:

$$C^p = \lambda_s \frac{A^p}{L^p} = \lambda_s \frac{V^p / L^p / CN}{L^p} \quad (7)$$

298 where  $\lambda_s$  is solid thermal conductivity,  $A^p$  is the cross-section area of the green cylinder,  $V^p$  is  
 299 the particle volume,  $L^p$  the distance from the particle centroid to the corresponding contact and  
 300  $CN$  is the coordination number of the target particle.

301 Similarly, calculations of thermal conductance  $C^{contact}$  used Eq. (8) via an interparticle  
 302 contact cylinder (orange cylinder in Fig. 5) with the corrected interparticle contact area  $A^C$   
 303 obtained from Eq. (6). The length of the contact cylinder was defined as  $3L^v$  ( $L^v$  is the pixel size  
 304 or voxel length) as suggested by [41] which was a validation of [42]. A coefficient  $\kappa$  was also  
 305 introduced in Eq. (8) to indicate the particle surface roughness since interparticle contact is a  
 306 combination of point-to-point contacts in real due to the surfaces roughness but are not  
 307 presented in CT images in Fig. 1 due to the physical limitation of the CT facility.  $\kappa$  was set as  
 308 0.75 since Askari et al. [43] concluded that the overestimation of the interparticle contact area  
 309 might be 25% if neglecting the effect of roughness.

$$C^{contact} = \lambda_s \frac{\kappa A^C}{3L^v} \quad (8)$$

310 The thermal conductance  $C^{gap}$  through the near-contacts is the sum of the thermal  
 311 conductance  $C^g$  (Eq. (9)) via each near-contact cylinder (light blue in Fig. 5). The cross-section  
 312 area of the cylinder is the area of a pixel ( $(L^v)^2$ ) with the length of the cylinder computed during  
 313 the identification process.

$$C^{gap} = \sum_l C_l^g = \lambda_v (L^v)^2 \sum_l \frac{1}{L_l^g} \quad (9)$$

314 The three conductance are combined to calculate the equivalent capacitance  $C_{ij}$  between the  
 315 centroid of particle  $i$  and  $j$  using Eq. (10). The  $C^{contact}$  is zero when two adjacent particles that  
 316 only have a near-contact (small gap).

$$C_{ij} = \left[ \frac{1}{C_i^p} + \frac{1}{(C^{contact} + C^{gap})} + \frac{1}{C_j^p} \right]^{-1} \quad (10)$$

317 The calculated  $C_{ij}$  using Eq. (10) was imported to Eq. (11)( the Fourier's law) to calculate  
 318 heat flux  $Q_{ij}$  using an open-source Python library, OpenPNM [44] as a function of the  
 319 temperature  $T$  in nodes  $i$  and  $j$ :

$$\sum_{i \rightarrow j} Q_{ij} = \sum_{i \rightarrow j} C_{ij}(T_i - T_j) \quad (11)$$

320 The temperatures on the opposite sides of the sample (inlet and outlet) were prescribed as  
 321  $T_{in} = 293$  K and  $T_{out} = 292$  K to create a small thermal gradient, with other boundaries simulated  
 322 as in thermally isolated conditions (or symmetrical,  $Q_{ij} = \text{nil}$  on these boundaries). The  $Q_{ij}$ ,  
 323 integrated on a cross-section perpendicular to the dominant heat transfer direction was selected  
 324 to calculate the  $\lambda_{eff}$  of the sample as:

$$ETC = \frac{\frac{1}{A} \sum Q_{ij}}{(T_{in} - T_{out})/L} \quad (12)$$

325 where  $A$  is the area of a selected cross-section,  $L$  is the length of the simulated sample.

326 Since the penalised interparticle contact area from Eq. (6) and a coefficient related to particle  
 327 surface roughness were used in Eq. (8) to calculate the thermal conductance at interparticle  
 328 contacts, TCNM has the merit of mitigating the overestimation of  $\lambda_{eff}$  caused by the partial  
 329 volume effect and particle surface roughness.

### 330 3.3.2 Effective thermal conductivity from physical testing

331 The selected sand samples were also poured into PVC containers with a height of 120 mm  
 332 and diameter of 50 mm using the same air-pluviation method to ensure consistency with the  
 333 samples used in CT scanning. A thermal needle probe with a length of 100 mm and diameter  
 334 of 2.4 mm was used to measure the  $\lambda_{eff}$  of each specimen following the ASTM standard D5334-  
 335 14 [21]. The PVC containers, whose size satisfy the requirement in ASTM standard, were also  
 336 scanned to check density consistency with the smaller axially loaded micro-CT scanned  
 337 samples.

## 338 4 Results and discussion

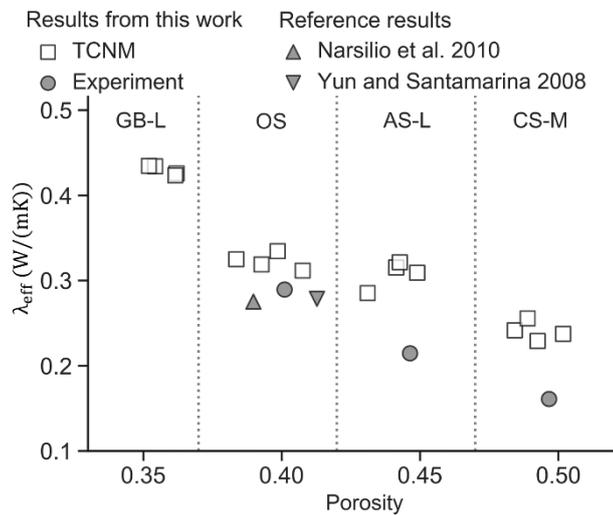
339 In this section, the TCNM is first validated for computing effective thermal conductivity  $\lambda_{eff}$   
 340 followed by a comprehensive discussion for selecting the important and non-redundant input  
 341 parameters for the ANN models. Since  $WCN_{ave}$  is a newly introduced mesoscale parameter,

342 the potential benefits of its inclusion in the prediction of  $\lambda_{eff}$  is investigated. Additionally, the  
 343 relationships between  $WCN_{ave}/WCN$  and traditional parameters are analysed for feature  
 344 reduction.

345 *4.1 Effective thermal conductivity results and TCNM validation*

346 From the CT images of each sand under no load, four small cubic ROIs with an edge length  
 347 of 4.55 mm were selected by cropping the CT images at different locations. The subsamples  
 348 are used for  $\lambda_{eff}$  and porosity calculations in TCNM and comparisons with physical testing.  
 349 Although the different grayscales in the CT images in Fig. 1 indicate minerals with different  
 350 densities and thermal conductivities in the sands, a fixed thermal conductivity (3 W/(mK))  
 351 previously used in papers [39, 45] was assigned to solids to eliminate the effect of mineral  
 352 composition, and isolate the effects of microstructures such as particle shape, connectivity and  
 353 porosity. The thermal conductivity of air was set as 0.025 W/(mK). Figure 6 illustrates that the  
 354  $\lambda_{eff}$  from the TCNM have a similar decreasing trend to the experimental results. The  $\lambda_{eff}$  using  
 355 the two methods are close for Ottawa sand (OS) while the  $\lambda_{eff}$  from TCNM is larger than  
 356 measurements for angular sand (AS-L) and crushed schist (CS-M). The main reason is that the  
 357 thermal conductivity of the solid phase in all samples are set same in TCNM simulation but  
 358 different in reality.

359



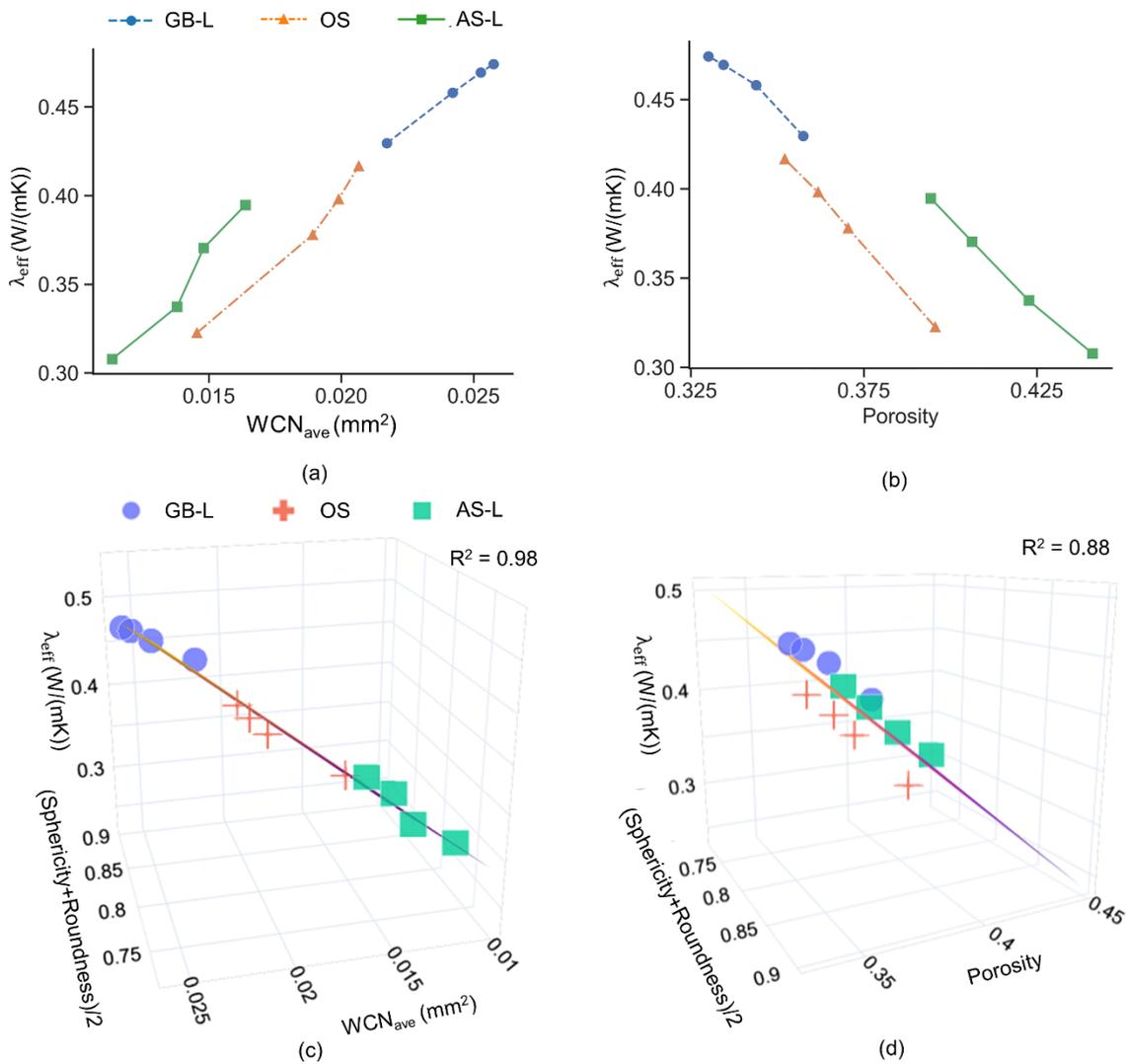
360

361 Fig. 6. The effective thermal conductivity computed from TCNM and validated by the experimental  
 362 results of glass beads (GB-L), Ottawa sand (OS), angular sand (AS-L) and crushed schist sand (CS-M).

## 363 4.2 Effect of $WCN_{ave}$ on effective thermal conductivity

364 The thermo-mechanical behaviour of granular materials under loads not only relates to the  
365 bulk properties such as porosity but also microstructural contact variables [14] such as the  
366  $WCN_{ave}$ . Therefore, the effect of  $WCN_{ave}$  on  $\lambda_{eff}$  should be investigated. For GB-L, OS and AS-  
367 L under stress levels of 0, 2, 6.1 and 10.2 MPa, the average  $\lambda_{eff}$  of the four subsamples in each  
368 sand were calculated. Fig. 7 (a) shows that their average  $\lambda_{eff}$  has a directly proportional  
369 relationship with the  $WCN_{ave}$ , in contrast to the inverse proportionality with porosity (Fig. 7  
370 (b)). The data from GB-L and OS in Fig. 7 (a) align along an overall trendline while the data  
371 in Fig. 7 (b) cluster in three groups. Since particles in the three sands have distinct shapes, Fig.  
372 7 (a) and Fig. 7 (b) were extended to include an additional dimension, by considering the  
373 average of sphericity and roundness in the third axis. Planes were also fitted to the data with  
374 calculated  $R^2$  in the 3D graphs shown in Fig. 7. Fig. 7 (c) shows that the  $R^2$  is high at 0.98,  
375 which indicates that the microscale geometrical parameters together with mesoscale  
376 topographic and contact quality variable can predict  $\lambda_{eff}$  well. If the macroscale porosity  
377 replaces the mesoscale  $WCN_{ave}$  as shown in Fig. 7 (d), the  $R^2$  decreases to 0.88, which suggests  
378 that porosity alone cannot characterise the microstructure. This also highlights the importance  
379 of mesoscale connectivity parameters in studies of sand thermo-mechanical responses.

380



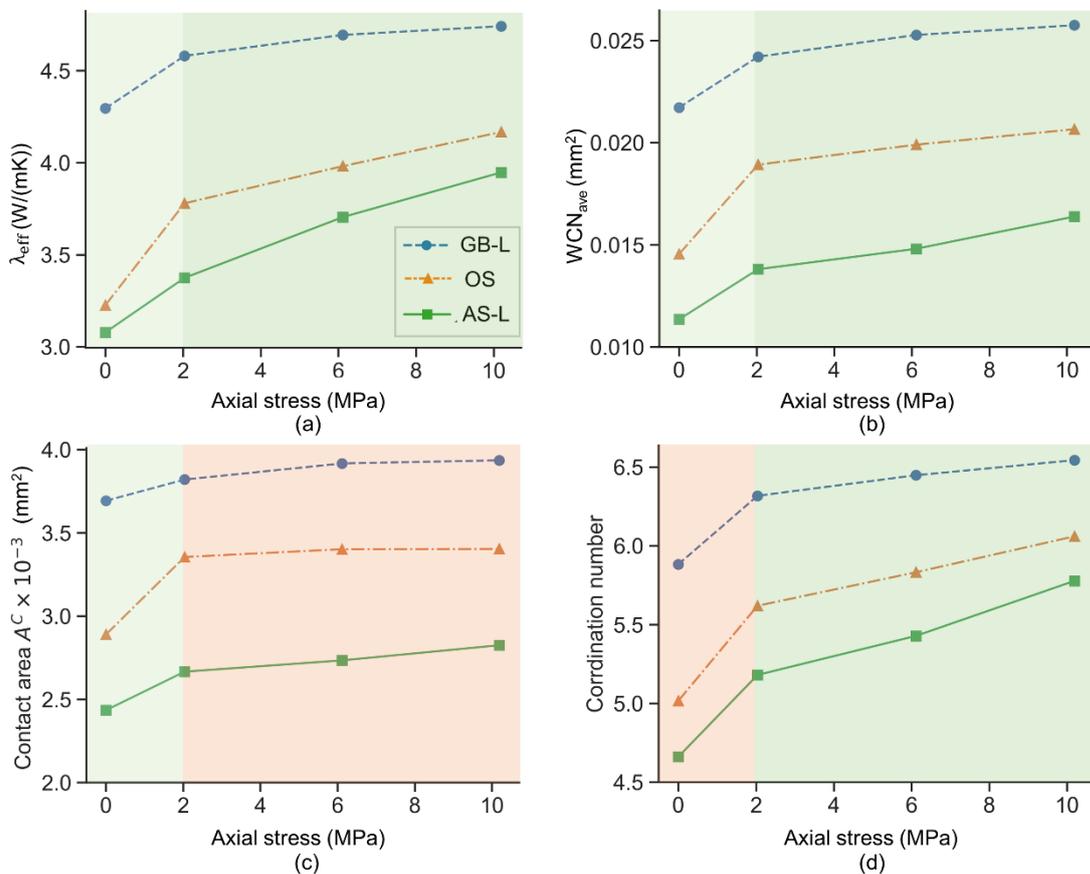
382

383 Fig. 7. The relationship between effective thermal conductivity and (a)  $WCN_{ave}$ , (b) porosity, (c)  
 384  $WCN_{ave}$  and particle shape, and (d) porosity and particle shape. (Click here to access the interactive  
 385 graphs).

### 386 4.3 Relationships between $WCN_{ave}$ / $WCN$ and traditional parameters

387 This section presents an analysis of why the  $WCN_{ave}$  can be an  $\lambda_{eff}$  predictor. From the  
 388 perspective of complex network theory, the  $WCN_{ave}$  unifies the coordination number  
 389 (connectivity) and contact area (as a weight in each edge of the network) as a single parameter.  
 390 While the axial stress under zero lateral strain on samples is *under 2 MPa*, Fig. 8 shows that  
 391 the slopes of the correlation between axial stress and  $\lambda_{eff}$  (Fig. 8 (a)) are similar to the slopes of  
 392 the relationship between axial stress and contact area for three soils (Fig. 8 (c)). The  $WCN_{ave}$   
 393 also has similar corresponding increasing slopes (Fig. 8 (b)). Although the coordination number  
 394 versus axial stress trends also increase, the gradients for OS and AS-L (for axial stress  $\leq 2$ MPa)

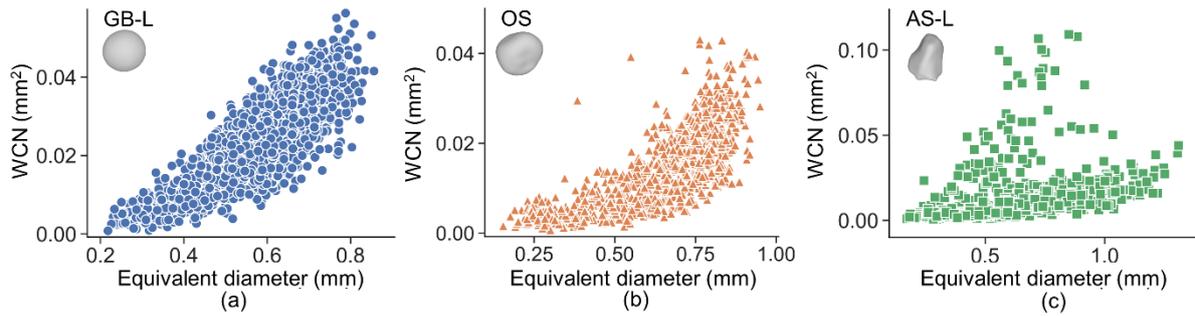
395 are different from the corresponding gradients observed in effective thermal conductivity  
 396 versus axial stress. The contact area shows a stagnant increase as the axial stress increases  
 397 beyond 2 MPa, (Fig. 8 (c)) which is no longer the same as the gradients observed in the  $\lambda_{eff}$   
 398 plots (Fig. 8 (a)). However, coordination numbers and the  $WCN_{ave}$  can capture the increase of  
 399  $\lambda_{eff}$  when the axial stress is larger than 2 MPa. In other words, the  $WCN_{ave}$  can closely follow  
 400 the increase of  $\lambda_{eff}$  over the whole range of axial stress since it captures the advantages of both  
 401 contact area and coordination number at different stages of axial stress. Fig. 8 (b) also shows  
 402 that the  $WCN_{ave}$  has a good relationship with axial stress for each sand and the value in  
 403 spherical GB-L is always the highest, which indicates that stress may be redundant and may  
 404 not be necessary for the ANN model to predict  $\lambda_{eff}$  if  $WCN_{ave}$  is used.  
 405



406  
 407 Fig. 8. Variation of (a) effective thermal conductivity, (b)  $WCN_{ave}$ , (c) average intercontact area  
 408 and (d) average coordination number with axial stress (and zero lateral strain).

409 As one of the main heat transfer processes is through particles in dry granular materials, the  
 410 particle diameter affects the heat transfer distance in the particle and the impact on  $WCN$  should  
 411 be explored. For GB-L, OS and AS-L under no load, particles in the four ROIs of each sand  
 412 (4,898 individual particles from 12 ROIs in total) were used to investigate the relationship

413 between the equivalent particle diameter and WCN. A clear and directly proportional  
 414 relationship between particle equivalent diameter and WCN can be seen in Fig. 9 (a) for  
 415 spherical GB-L, which is reasonable since a large particle has a higher opportunity to touch  
 416 more particles and a larger total contact area once touching. The positive trend also exists in  
 417 Fig. 9 (b) and Fig. 9 (c) for more irregular OS and AS-L sands even though there is a divergence  
 418 in Fig. 9 (c). Therefore, the equivalent particle diameter is unnecessary to be involved in the  
 419 ANN model on top of the WCN for  $\lambda_{eff}$  prediction due to their intercorrelation.

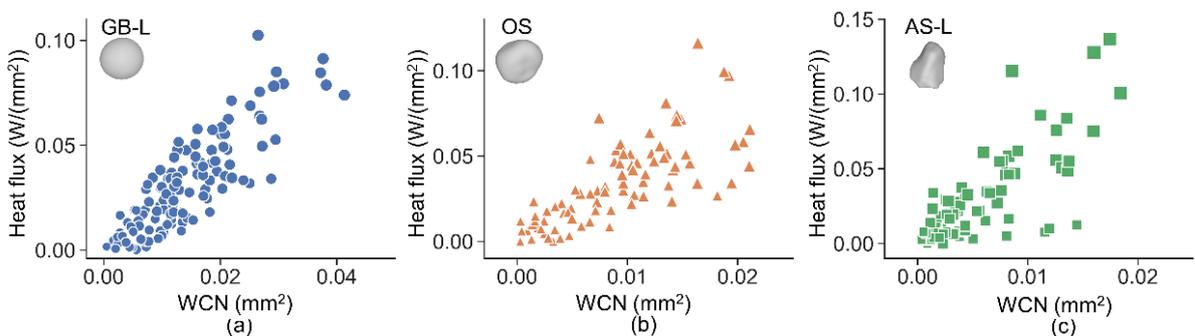


420

421 Fig. 9. The dependence of WCN on equivalent particle diameter for three selected sands

#### 422 4.4 Effect of WCN on heat flux

423 Since heat flux was used in Eq. (11) to compute  $\lambda_{eff}$ , the particles at the inlet and outlet of a  
 424 subsample in each sand were used to study the relationship between WCN and heat flux. The  
 425 heat flux from the centroid of a particle to the centroid of all its neighbours was calculated in  
 426 the TCNM, showing positive correlations to WCN displayed in Fig 10. The clear relationship  
 427 is because the WCN considers contact area which was used to calculate thermal conductance  
 428 (Eq. (8)) and further served the computation of heat flux using the Fourier's law. Similar to  
 429 Figure 9, the correlation is clearest in the spherical GB-L and becomes weaker in more irregular  
 430 sands.



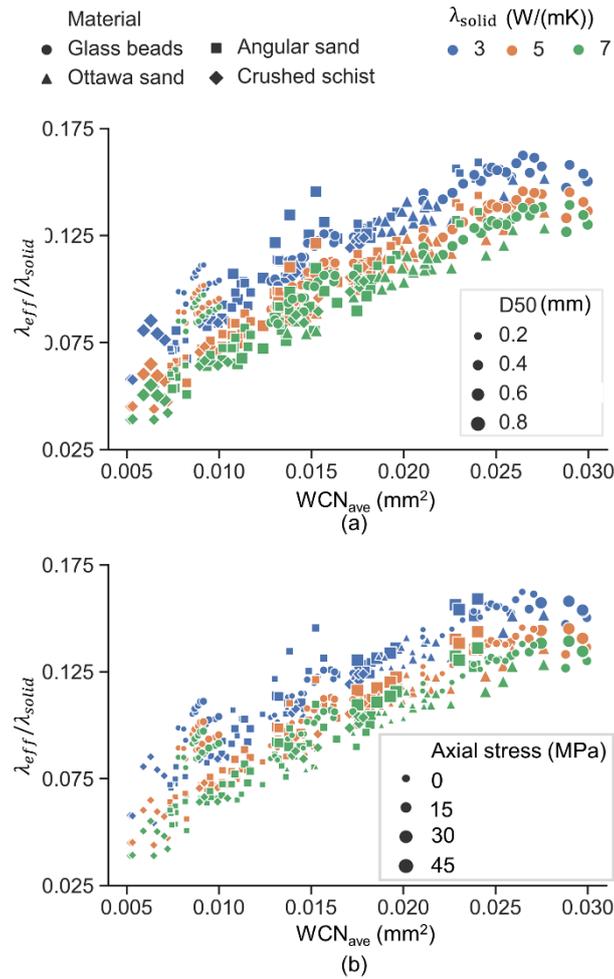
431

432 Fig. 10. The relationship between the total heat flux and WCN of particles at inlet and outlet in three  
 433 selected sands

#### 434 4.5 ANN model construction

435 Only a small subset of all samples was used in the above analyses (those shown in bold in  
436 Table 2). Data from more samples are required to construct an ANN model. Four subsamples  
437 (ROIs) from all 152 samples in Table 2 were selected and the solid material of each particle in  
438 each ROI was assigned three different thermal conductivities, to render 456 datapoints used for  
439 the ANN model. The average 3D sphericity, 3D roundness,  $WCN_{ave}$ , porosity and  $\lambda_{eff}$  under a  
440 larger range of loads (up to 40.7 MPa) for these samples were calculated. In addition to setting  
441 the thermal conductivity of the solid phase as 3 W/(mK), 5 and 7 W/(mK) were also used for  
442 enriching the database. Although dimensionless  $\lambda_{eff}/\lambda_{solid}$  instead of  $\lambda_{eff}$  was used as the output  
443 of the ANN model, the data in Fig. 11 (a) whose markers were rendered by  $\lambda_{solid}$  still shows  
444 three distinct cluster groups that correspond to different  $\lambda_{solid}$ . Therefore, the ANN model also  
445 requires  $\lambda_{solid}$  as an input parameter. The markers in Fig. 11 (a) represent different sands and  
446 the size of the markers indicates the equivalent average particle diameter of the subsample.  
447 Figure 11 (b) presents the same data as Fig. 11 (a) but the markers show the loadings applied  
448 to the subsamples. The data were randomly split into a training set (80%), validation set (10%)  
449 and a testing set (10%).

450

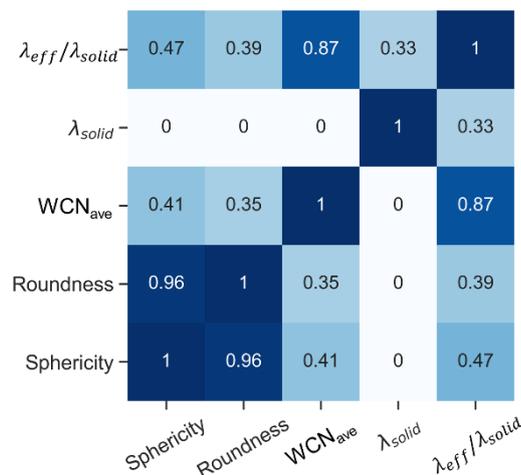


451

452 Fig. 11. The database used to construct the ANN model.

#### 453 4.5.1 ANN model I: $\lambda_{solid}$ , sphericity, roundness and $WCN_{ave}$ as input parameters

454 Packing structure models [46] are a type of models that use particle topology to predict  $\lambda_{eff}$ .  
 455 However, few studies have been conducted except measuring particle connectivity using  
 456 Voronoi tessellation [47], typical lattice structure [48] or bond orientation [49]. Since the  
 457  $WCN_{ave}$  can quantify the structure of granular materials, ANN model I used  $\lambda_{solid}$ , sphericity,  
 458 roundness and the  $WCN_{ave}$  (but not porosity) as input parameters and  $\lambda_{eff}/\lambda_{solid}$  as the output to  
 459 imitate the *packing structure models* [46]. Figure 12 shows that sphericity and roundness  
 460 display a good correlation to each other with  $R^2$  of 0.96 for the four tested sands. Still, complete  
 461 coverage of the wide range of irregular particle shapes requires both parameters, as shown in  
 462 [33]. The  $R^2$  of the correlation between each pair of the particle shape descriptors,  $WCN_{ave}$  and  
 463  $\lambda_{solid}$  in Fig. 12 are not high, which implies that these input parameters are not redundant for  
 464 ANN model I. The  $R^2$  of the relationship between  $WCN_{ave}$  and  $\lambda_{eff}/\lambda_{solid}$  is 0.87, and indicates  
 465 that interparticle connectivity and contact quality play crucial roles in the heat transfer of dry  
 466 granular materials.



468

469 Fig. 12. A heatmap presents the  $R^2$  between each pair of features used in ANN model I

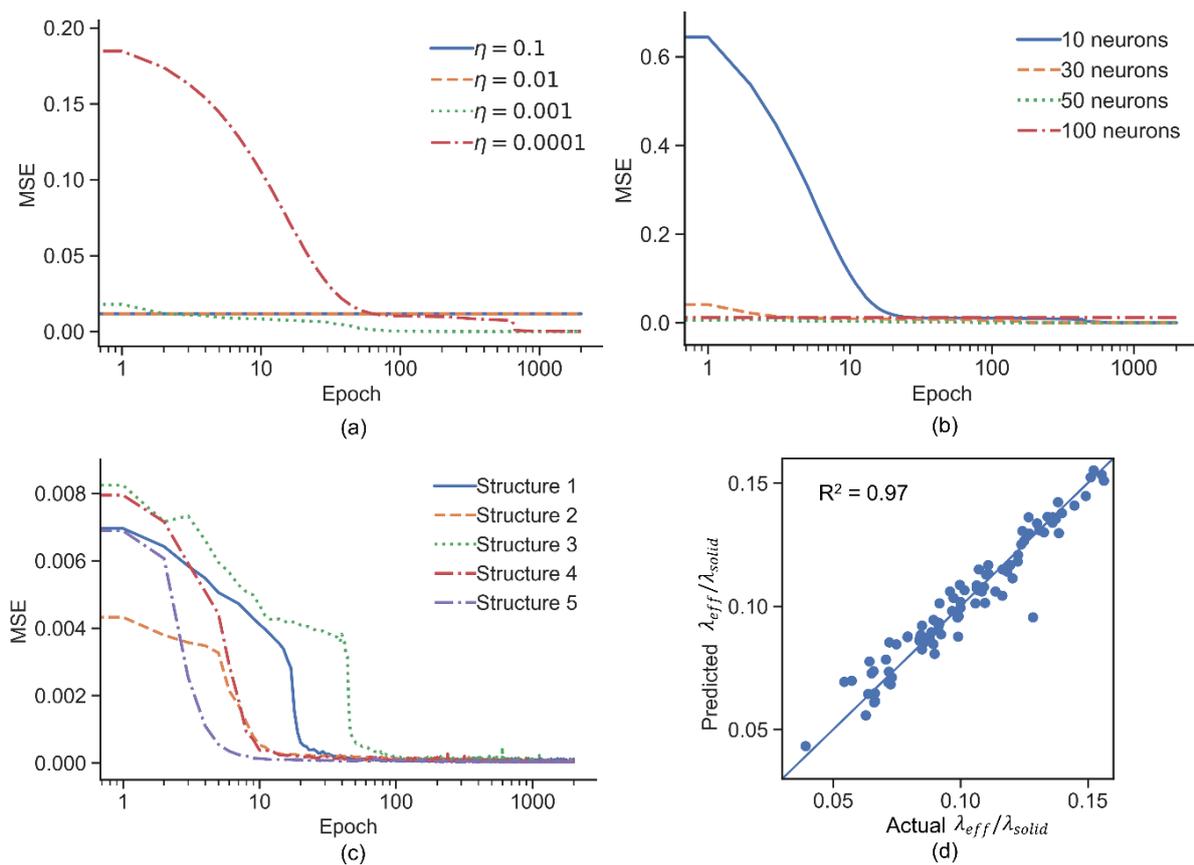
470

471 The ANN is suitable for numerous complex problems due to its flexibility, which is also  
 472 one of its main drawbacks [30]. Values of model and algorithm parameters (i.e.,  
 473 hyperparameters) should be decided since any imaginable network topologies can be used. This  
 474 study tuned the learning rate  $\eta$ , the neuron number in the hidden layer, and the structure  
 475 indicating how neurons are interconnected to find the desirable ANN model. MSE was used to  
 476 monitor the error during the training processes until *epoch* reached 2,000. An epoch is one  
 477 cycle that the model learns through the full training dataset.

478 The effect of learning rate  $\eta$  and neuron number on the performance of the ANN model I  
 479 with one hidden layer was first studied. The ANN model with different learning rates  $\eta =$   
 480 0.1, 0.01, 0.001, 0.0001 and a constant 30 neurons in the single hidden layer was trained. The  
 481 large learning rates such as  $\eta = 0.1, 0.01$  seen in Figure 13 (a), boosted the ANN model and  
 482 displayed low MSE even at the very beginning of training. However, the MSE maintained the  
 483 same level until the end of training. By contrast,  $\eta = 0.001$  can reach a low MSE which is  
 484 similar to the MSE when  $\eta = 0.0001$ , and converge at an earlier stage. Therefore,  $\eta = 0.001$   
 485 , a commonly used value [30], was selected as the learning rate for the ANN model I. Next, the  
 486 neuron number was tuned in the single hidden ANN model with the learning rate  $\eta = 0.001$ .  
 487 Figure 13 (b) shows that the ANN model with more neurons requires a longer training time.  
 488 Here we chose 30 neurons in a hidden layer to balance efficiency and accuracy. In the next  
 489 study, five structures [50], [50,30], [50, 30, 10], [100, 50, 30], [100, 50, 30, 10] with  $\eta = 0.001$   
 490 were implemented to analyse the effect of interconnection of neurons on the performance of  
 491 ANN model. A structure indicates the number of hidden layers and the number of neurons in

492 each hidden layer. For example, the second structure [50, 30] means that an ANN model has  
 493 two hidden layers, the first hidden layer has 50 neurons while the second hidden layer has 30  
 494 neurons. It can be observed from Fig. 13 (c) that the second structure is appropriate for ANN  
 495 model I since it is relatively simple and its MSE converges at a medium rate. The converged  
 496 MSE in Fig. 13 (c) is smaller than that in Fig. 13 (a) and Fig. 13 (b) by two orders of magnitude,  
 497 which hints at the importance of a proper structure for an ANN model. Since the converged  
 498 MSE in Fig. 13 (c) is also much smaller than the  $\lambda_{eff}/\lambda_{solid}$  as shown in Fig. 11, the tuned  
 499 hyperparameters were believed to be a proper combination for ANN model I. Finally, the  
 500 testing dataset was used to predict  $\lambda_{eff}/\lambda_{solid}$  and compared with the ‘true’ values as shown in  
 501 Fig. 13 (d). The predicted values have a high correlation ( $R^2=0.97$ ) with the actual values,  
 502 indicating that the  $WCN_{ave}$  and particle shape characteristics can be used as variables in packing  
 503 structure models to predict  $\lambda_{eff}/\lambda_{solid}$  well.

504

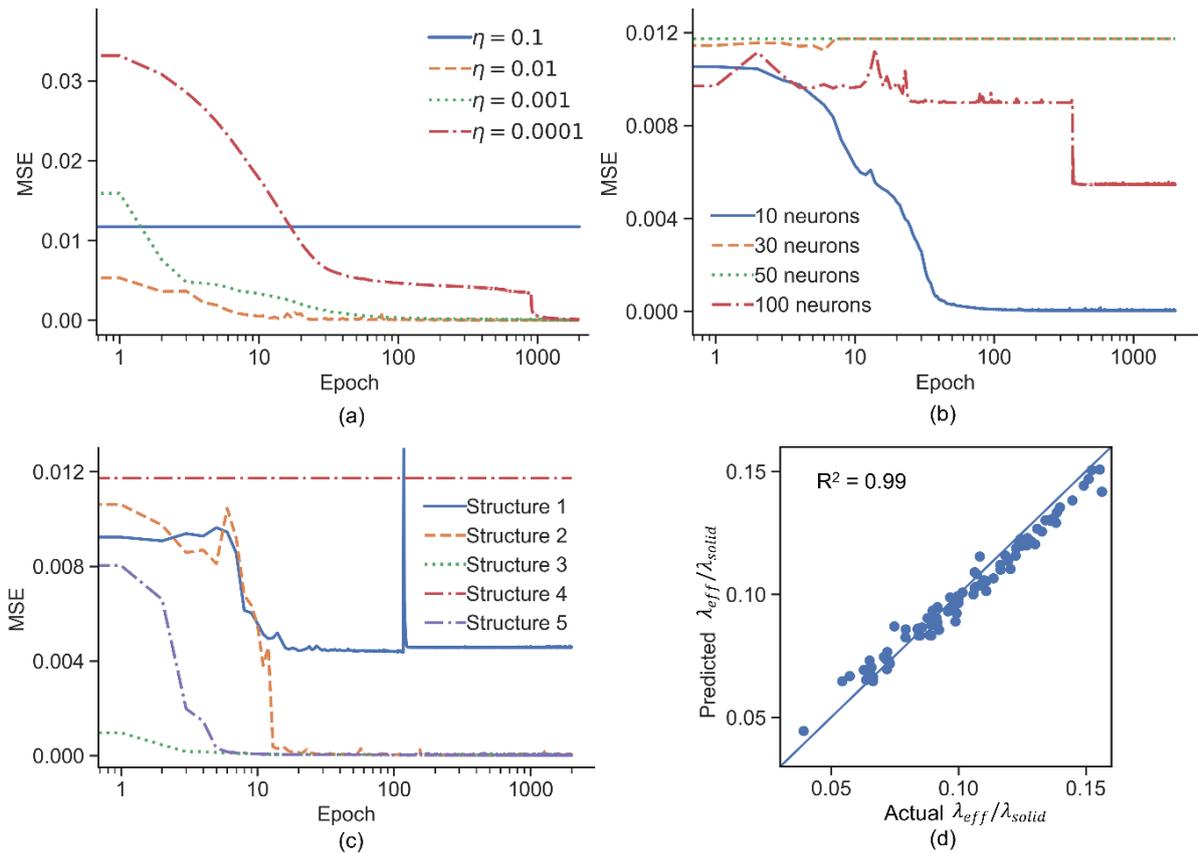


505

506 Fig. 13. Tuning learning rate  $\eta$  (a), neuron number in the hidden layer (b) and structure (c) for ANN  
 507 model I. The correlation between the actual effective thermal conductivity and predicted effective  
 508 thermal conductivity using the tuned ANN model I on the testing set is show in (d).

509 4.5.2 ANN model II:  $\lambda_{solid}$ , sphericity, roundness,  $WCN_{ave}$  and porosity as input parameters

510 ANN model I considered only microscale and mesoscale parameters. An ANN model II  
511 uses a macroscopic parameter, porosity, in addition to those. In ANN model I, sphericity and  
512 roundness are among the input parameters that describe the geometry of a particle, and capture  
513 information from granular materials at particle-scale (microscale). The  $WCN_{ave}$  quantifies the  
514 particle connectivity and contact quality (mesoscale) but does not quantify the whole sample  
515 generally as the bulk properties do at macroscale. Porosity, a bulk property, is used in  
516 ANN model II to include a variable at the sample scale (macroscale). Hence, ANN model II  
517 involves input parameters across all scales. After using the similar tuning processes for  
518 hyperparameters as shown in Fig. 14 (a)-(c), the same structure No.2 [50,30] with learning rate  
519  $\eta = 0.001$  were also selected for ANN model II. Figure 14 (d) presents that the  $R^2$  of the  
520 relationship between the predicted and actual  $\lambda_{eff}/\lambda_{solid}$  is 0.99, which is higher than ANN model  
521 I. The porosity as a new input parameter in ANN model II, quantifies the void fraction and  
522 loosely indicates the number of particles in a sample. Higher particle counts mean more  
523 potential heat transfer pathways in granular assemblies. As explained in previous sections,  
524 other parameters also relate to heat transfer mechanisms and capture three diverse aspects: (1)  
525  $\lambda_{solid}$  determines the heat transfer efficiency within particles; (2) sphericity and roundness  
526 indicate interparticle contact quality and (3) the  $WCN_{ave}$  measures particle connectivity and  
527 interparticle contact quality, and also relates to particle diameter (the heat transfer pathway  
528 within particles) and thermal conductance. Capturing abundant microstructural information  
529 that influence heat transfer certainly results in an accurate  $\lambda_{eff}$  prediction. Consequently, we  
530 conclude that considering multiscale microstructural parameters at different scales in  $\lambda_{eff}$   
531 models can result in an accurate  $\lambda_{eff}$  prediction. Supplementary files with the two ANN models  
532 (ANN-Model-I.h5 and ANN-Model-II.h5) have been included in this paper for readers to use.  
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Fig. 14. Tuning learning rate  $\eta$  (a), neuron number in the hidden layer (b) and structure (c) for the ANN model II. The correlation between the actual effective thermal conductivity and predicted effective thermal conductivity using the tuned ANN model II.

## 538 5 Conclusions

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Microstructure and boundary conditions (e.g., axial loading) in granular materials control  $\lambda_{eff}$ , but microstructural parameters are seldomly used in existing  $\lambda_{eff}$  models, perhaps with the exceptions of (global) porosity and aspect ratio. The advancement of new techniques such as CT, complex network theory, and new numerical simulation methods enable access to the microstructure of natural sands and promote a need for data-driven approaches, for example with the advancement of machine learning techniques, to predict  $\lambda_{eff}$  accurately and efficiently.

Four dry sand assemblies varying in particle size, shape and under different stress levels were CT scanned to achieve image stacks. By applying image processing methods to the image stacks, microstructural parameters such as particle size, 3D sphericity and roundedness and porosity were obtained. In addition, the contact network was constructed to calculate the WCN according to complex network theory. The applicability of these parameters to the ANN model was justified by the analysis of heat transfer mechanism, review of  $\lambda_{eff}$  models and their interplay. The utilisation of microstructural parameters provides the ANN model with some

552 physically-based preconditioning, rather than utilising an ANN model merely as a black-box  
553 with somehow random input parameters. Finally, the results indicate that the ANN model,  
554 which considers multiple-scale microstructural parameters can predict  $\lambda_{eff}$  well, with best  
555 predictions using parameters that characterise granular materials across scales:  $\lambda_{solid}$ , *sphericity*,  
556 *roundness* (at the particle scale), *WCN* (at the mesoscale) and *porosity* (at the macroscale)

557 This work proves the feasibility of applying ANN to material science, particularly for  
558 predictions of  $\lambda_{eff}$ . The physics-based data-driven approach allows the acceleration of material  
559 design in a more autonomous and objective process. This paper uses the WCN from a contact  
560 network since it is easier to estimate than other mesoscale network features [15]. However, the  
561 WCN from the contact network only considers the interparticle contacts but not near-contacts  
562 which can be involved in thermal network features [15]. The authors are striving to merge the  
563 several aforementioned techniques into a platform which can enable the academic community  
564 to achieve microstructural parameters including thermal network features easily and  
565 conveniently. Future work includes continuing to increase the current database of granular  
566 materials of different shapes and to explore ANN models built with thermal network features  
567 and non-dry materials.

## 568 **Declaration of competing interest**

569 The authors declared that there is no conflict of interest.

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## 578 **References**

- 579 [1] C. Pasten, J.C. Santamarina, Thermally induced long-term displacement of thermoactive piles,  
580 *Journal of Geotechnical and Geoenvironmental Engineering*, 140(5) (2014) 06014003.  
581 [2] D.M. Scott, D.K. Das, V. Subbaihaannadurai, V.A. Kamath, A computational scheme for fluid flow  
582 and heat transfer analysis in porous media for recovery of oil and gas, *Petroleum science and*  
583 *technology*, 23(7-8) (2005) 843-862.

584 [3] W.B. Fei, Q. Li, X.C. Wei, R.R. Song, M. Jing, X.C. Li, Interaction analysis for CO<sub>2</sub> geological  
585 storage and underground coal mining in Ordos Basin, China, *Engineering geology*, 196 (2015) 194-  
586 209.

587 [4] M. Moscardini, Y. Gan, S. Papeschi, M. Kamlah, Discrete element method for effective thermal  
588 conductivity of packed pebbles accounting for the Smoluchowski effect, *Fusion Engineering and*  
589 *Design*, 127 (2018) 192-201.

590 [5] D.N. Singh, K. Devid, Generalized relationships for estimating soil thermal resistivity, *Experimental*  
591 *Thermal and Fluid Science*, 22(3) (2000) 133-143.

592 [6] S. Zhao, J. Zhao, Y. Lai, Multiscale modeling of thermo-mechanical responses of granular materials:  
593 A hierarchical continuum–discrete coupling approach, *Computer Methods in Applied Mechanics and*  
594 *Engineering*, 367 (2020) 113100.

595 [7] W. Fei, G.A. Narsilio, Network analysis of heat transfer in sands, *Computers and Geotechnics*  
596 (2020).

597 [8] S. Zhao, J. Zhao, N. Guo, Universality of internal structure characteristics in granular media under  
598 shear, *Physical Review E*, 101(1) (2020) 012906.

599 [9] W.d. van Antwerpen, C. Du Toit, P. Rousseau, A review of correlations to model the packing  
600 structure and effective thermal conductivity in packed beds of mono-sized spherical particles, *Nuclear*  
601 *Engineering and design*, 240(7) (2010) 1803-1818.

602 [10] Z. Abdulagatova, I. Abdulagatov, V. Emirov, Effect of temperature and pressure on the thermal  
603 conductivity of sandstone, *International Journal of Rock Mechanics and Mining Sciences*, 46(6) (2009)  
604 1055-1071.

605 [11] A.M. Abyzov, A.V. Goryunov, F.M. Shakhov, Effective thermal conductivity of disperse  
606 materials. I. Compliance of common models with experimental data, *International Journal of Heat and*  
607 *Mass Transfer*, 67 (2013) 752-767.

608 [12] R. Askari, S.H. Hejazi, M. Sahimi, Effect of deformation on the thermal conductivity of granular  
609 porous media with rough grain surface, *Geophysical Research Letters*, 44(16) (2017) 8285-8293.

610 [13] N. Yüksel, The review of some commonly used methods and techniques to measure the thermal  
611 conductivity of insulation materials, in: *Insulation materials in context of sustainability*, IntechOpen,  
612 2016.

613 [14] R.K. Desu, A.R. Peeketi, R.K. Annabattula, Artificial neural network-based prediction of effective  
614 thermal conductivity of a granular bed in a gaseous environment, *Computational Particle Mechanics*,  
615 6(3) (2019) 503-514.

616 [15] W. Fei, G.A. Narsilio, J.H. van der Linden, M.M. Disfani, Network analysis of heat transfer in  
617 sphere packings, *Powder Technology*, 362 (2020) 790-804.

618 [16] L. Papadopoulos, M.A. Porter, K.E. Daniels, D.S. Bassett, Network analysis of particles and grains,  
619 *Journal of Complex Networks*, 6(4) (2018) 485-565.

620 [17] G.A. Narsilio, J. Kress, T.S. Yun, Characterisation of conduction phenomena in soils at the particle-  
621 scale: Finite element analyses in conjunction with synthetic 3D imaging, *Computers and Geotechnics*,  
622 37(7) (2010) 828-836.

623 [18] J. Gan, Z. Zhou, A. Yu, Effect of particle shape and size on effective thermal conductivity of  
624 packed beds, *Powder Technology*, 311 (2017) 157-166.

625 [19] W.-Z. Fang, H. Zhang, L. Chen, W.-Q. Tao, Numerical predictions of thermal conductivities for  
626 the silica aerogel and its composites, *Applied Thermal Engineering*, 115 (2017) 1277-1286.

627 [20] H. Wei, S. Zhao, Q. Rong, H. Bao, Predicting the effective thermal conductivities of composite  
628 materials and porous media by machine learning methods, *International Journal of Heat and Mass*  
629 *Transfer*, 127 (2018) 908-916.

630 [21] ASTM D5334-14, Standard Test Method for Determination of Thermal Conductivity of Soil and  
631 Soft Rock by Thermal Needle Probe Procedure, in, *ASTM International*, West Conshohocken, PA,  
632 2014.

633 [22] S. Ju, J. Shiomi, *Materials Informatics for Heat Transfer: Recent Progresses and Perspectives*,  
634 *Nanoscale and Microscale Thermophysical Engineering*, 23(2) (2019) 157-172.

635 [23] E.J. Kautz, A.R. Hagen, J.M. Johns, D.E. Burkes, A machine learning approach to thermal  
636 conductivity modeling: A case study on irradiated uranium-molybdenum nuclear fuels, *Computational*  
637 *Materials Science*, 161 (2019) 107-118.

638 [24] N. Zhang, H. Zou, L. Zhang, A.J. Puppala, S. Liu, G.J.I.J.o.T.S. Cai, A unified soil thermal  
639 conductivity model based on artificial neural network, 155 (2020) 106414.

640 [25] H. Wei, H. Bao, X. Ruan, Machine learning prediction of thermal transport in porous media with  
641 physics-based descriptors, *International Journal of Heat and Mass Transfer*, 160 (2020) 120176.

642 [26] B. Yan, R. Gao, P. Liu, P. Zhang, L. Cheng, Optimization of thermal conductivity of UO<sub>2</sub>-Mo  
643 composite with continuous Mo channel based on finite element method and machine learning,  
644 *International Journal of Heat and Mass Transfer*, 159 (2020) 120067.

645 [27] W. Fei, G.A. Narsilio, J.H. van der Linden, M.M. Disfani, Quantifying the impact of rigid  
646 interparticle structures on heat transfer in granular materials using networks, *International Journal of*  
647 *Heat and Mass Transfer*, 143 (2019) 118514.

648 [28] J.H. van der Linden, G.A. Narsillio, T. Antoinette, Thermal conductance network model for  
649 computerised tomography images of real geomaterials (Conditionally accepted), *Computers and*  
650 *Geotechnics*, (2019).

651 [29] M. Wiebicke, E. Andò, I. Herle, G. Viggiani, On the metrology of interparticle contacts in sand  
652 from x-ray tomography images, *Measurement Science and Technology*, 28(12) (2017) 124007.

653 [30] A. Géron, *Hands-On Machine Learning with Scikit-Learn, Keras, and TensorFlow: Concepts,*  
654 *Tools, and Techniques to Build Intelligent Systems*, O'Reilly Media, 2019.

655 [31] B. Mwangi, T.S. Tian, J.C.J.N. Soares, A review of feature reduction techniques in neuroimaging,  
656 12(2) (2014) 229-244.

657 [32] T.S. Yun, J.C. Santamarina, Fundamental study of thermal conduction in dry soils, *Granular matter*,  
658 10(3) (2008) 197-207.

659 [33] W. Fei, G.A. Narsilio, M.M. Disfani, Impact of three-dimensional sphericity and roundness on  
660 heat transfer in granular materials, *Powder Technology*, 355 (2019) 770-781.

661 [34] H. Shin, J. Santamarina, Role of particle angularity on the mechanical behavior of granular  
662 mixtures, *Journal of Geotechnical and Geoenvironmental Engineering*, 139(2) (2013) 353-355.

663 [35] P. Zehner, E.U. Schlunder, Thermal Conductivity of Granular Materials at Moderate Temperatures,  
664 *Chemie. Ingr-Tech.*, 42 (1970) 933-941.

665 [36] H. Fricke, A mathematical treatment of the electric conductivity and capacity of disperse systems  
666 I. The electric conductivity of a suspension of homogeneous spheroids, *Physical Review*, 24(5) (1924)  
667 575.

668 [37] T. Keller, U. Motschmann, L. Engelhard, Modelling the poroelasticity of rocks and ice,  
669 *Geophysical prospecting*, 47(4) (2001) 509-526.

670 [38] N. Otsu, A threshold selection method from gray-level histograms, *IEEE transactions on systems,*  
671 *man, and cybernetics*, 9(1) (1979) 62-66.

672 [39] T.S. Yun, T.M. Evans, Three-dimensional random network model for thermal conductivity in  
673 particulate materials, *Computers and Geotechnics*, 37(7) (2010) 991-998.

674 [40] T.P. Peixoto, The graph-tool python library, *figshare*, (2014).

675 [41] M. Shapiro, V. Dudko, V. Royzen, Y. Krichevets, S. Lekhtmakher, V. Grozubinsky, M. Shapira,  
676 M. Brill, Characterization of Powder Beds by Thermal Conductivity: Effect of Gas Pressure on the  
677 Thermal Resistance of Particle Contact Points, *Particle & Particle Systems Characterization*, 21(4)  
678 (2004) 268-275.

679 [42] R. Bauer, E. Schlunder, Effective radial thermal-conductivity of packings in gas flow, part -ii:  
680 Thermal conductivity of packing fraction without gas flow, *International Chemical Engineering*, 18(2)  
681 (1978) 189-204.

682 [43] R. Askari, S. Taheri, S.H. Hejazi, Thermal conductivity of granular porous media: A pore scale  
683 modeling approach, *AIP Advances*, 5(9) (2015).

684 [44] J.T. Gostick, Versatile and efficient pore network extraction method using marker-based watershed  
685 segmentation, *Physical Review E*, 96(2) (2017) 023307.

686 [45] J. Sundberg, P.-E. Back, L.O. Ericsson, J. Wrafter, Estimation of thermal conductivity and its  
687 spatial variability in igneous rocks from in situ density logging, *International Journal of Rock*  
688 *Mechanics and Mining Sciences*, 46(6) (2009) 1023-1028.

689 [46] J. Mo, H. Ban, Measurements and theoretical modeling of effective thermal conductivity of particle  
690 beds under compression in air and vacuum, *Case studies in thermal engineering*, 10 (2017) 423-433.

691 [47] J. Finney, Random packings and the structure of simple liquids. I. The geometry of random close  
692 packing, *Proc. R. Soc. Lond. A*, 319(1539) (1970) 479-493.

- 693 [48] W. Siu, S.-K. Lee, Effective conductivity computation of a packed bed using constriction resistance  
694 and contact angle effects, *International journal of heat and mass transfer*, 43(21) (2000) 3917-3924.  
695 [49] W. Dai, D. Hanaor, Y. Gan, The effects of packing structure on the effective thermal conductivity  
696 of granular media: A grain scale investigation, *International Journal of Thermal Sciences*, 142 (2019)  
697 266-279.  
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